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Load Flow Solution for Radial Networks with Composite and Exponential Loads

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ABSTRACT: A network-topology-based method is used to solve the load-flow problem of radial distribution networks in this Thesis. Power flow equations in matrix form are developed based on the topology. The technique requires line data in such way that the receiving end node must be in an ascending order. The implemented method requires building of two matrices: BIBC and branch-current to bus-voltage (BCBV) matrix. The bus-injection to branch-current (BIBC) is built by assigning unity to the nodes of the discovered paths. The method requires less number of iterations i.e., maximum of 3 iterations for convergence. In this Thesis, constant power load, constant current load, constant impedance load, composite and exponential loads have been considered for load flow solution. Load flow is obtained for 15 Bus, 33 Bus, 69 Bus and 85 Bus Systems. Load flow results are presented for various systems and also presented in graphical form. Results obtained for various types of loads are compared with the established results in the literature. They are found to be accurate to the third digit. Load flow algorithm is implemented in MATLAB.

KEYWORDS: Radial networks, Load flow, Bus system, Topology, MATLAB.

I.INTRODUCTION

Load flow analysis of distribution systems has not received much attention unlike load flow analysis of transmission systems. However, some work has been carried out on load flow analysis of a distribution network but the choice of a solution method for a practical system is often difficult. Generally distribution networks are radial and the R/X ratio is very high. Because of this, distribution networks are ill-conditioned and conventional Newton-Raphson (NR) and fast decoupled load flow (FDLF) methods are inefficient at solving such networks. Many researchers have suggested modified versions of the conventional load flow methods for solving ill-conditioned power networks. Recently researchers have paid much attention obtaining the solution of distribution networks. In India, all the 11 kV rural distribution feeders are radial and too long. The voltages at the far end of many such feeders are very low with very high voltage regulation. In this project, the main aim has been to implement a load flow technique for radial distribution networks. This method involves construction of two network matrices based on topology and matrix operations. Computationally this method is very efficient. Another advantage of this method is that it requires less computer memory. Convergence is always guaranteed for any type of practical radial distribution network with a realistic R/X ratio while using this method. Loads, in the present formulation, have been represented as constant power. However, this method can easily include composite load modeling if the break up of the loads is known. This load flow technique has been implemented using MATLAB. Several practical rural radial distribution feeders in India have been successfully solved using this method. In this paper, only 10 bus unbalanced system is considered. Relative speed and memory requirements of this load flow method are better than method proposed by Baran and Wu as per the literature.

Distribution system provides a final link between high voltage transmission systems and consumer services. The power loss is significantly high in distribution systems because of lower voltages and higher currents, when compared to that in high voltage transmission systems. Studies have indicated that as much as 13% of total power generated is consumed as I^2R losses in distribution level. Reactive currents account for a portion of these losses. Reduction of total loss in distribution systems is very essential to improve the overall efficiency of power delivery. The pressure of improving the overall efficiency of power delivery has forced the power utilities to reduce the loss, especially at



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Vol. 6, Issue 12, December 2017

distribution level. In recent years, considerable attention has been focused in planning of a distribution system, to reduce the power and energy losses, to reduce the capital investment involved and to provide better quality supply to consumers. Improved modeling techniques and certain optimization and programming approaches have been presented to determine the best location, and suitable interconnections between sub-stations so as to meet the increasing demands more reliably and economically. In these approaches, shunt capacitors are introduced to reduce losses and to provide reactive power compensation. A Distribution system is one from which the power is distributed to various users through feeders, distributors and service mains. Feeders are conductors of large current carrying capacity, carrying the current in bulk to the feeding points. Distributors are conductors from which the current is tapped off for supply to the consumer premises. The size of feeder is determined primarily by the currents it is required to carry, and on the other hand the permissible voltage along a distributor forms the main basis of design in case of a distributor. The size and cross-section, of feeders and distributors are affected by the increase in supply voltage. It has been established that 70% of the total system losses are occurring in the primary and secondary distribution system, while transmission and sub-transmission lines account for only 30% of the total losses. Therefore the primary and secondary distribution systems must be properly planned to ensure losses within the acceptable limits.

Distribution Automation Systems have evolved both in concept and implementation over a period of time. The distribution power flow has influenced other applications such as network optimization, VAR planning and switching. The distribution systems, characterized by their prevailing radial nature and high r/x ratio, render them to be ill-conditioned and make the traditional Newton-Raphson (NR) and fast decoupled power flow (FDPF) solution techniques unsuitable. Consequently many power flow algorithms specially suited for distribution systems have emerged and are well documented. These methods are roughly viewed as node based and branch based methods. The first category has used node voltages or current injections as state variables and requires information on the derivatives of network equations. Abul Wafa et al have used a graphical approach for developing loadflow equations in matrix form to satisfy the need of distribution automation. Depth first search is used to trace the path of power flow direction. Matrices are developed based on discovered path [1]. Teng and Lin developed topology based load flow solution [2]. A simple power flow method for radial distribution networks proposed by Das et al involves evaluation of simple algebraic expressions of the receiving-end voltages. No importance is given for initial guess solution in Das et al and other related research works [3]. Shirmohammadi et al have presented a compensation-based power flow method for weakly meshed distribution and transmission systems [4]. Stevens et al have shown that the ladder technique is found to be fastest but did not converge in five out of 12 cases studied [5]. Goswami and Basu have presented a direct solution method for solving radial and meshed distribution networks [6]. Jasmon and Lee have derived the fundamental equations for solving a load flow problem of a distribution network using a single-line equivalent [7]. Goswami and Ghosh have presented a direct method for solving radial and mesh distribution networks [8]. Haque has proposed a method suitable for both radial and mesh configurations. It being a Z-bus based method, the sparsity structure cannot be exploited which is the greatest disadvantage. Das et al have suggested a load flow solution for meshed distribution networks only. The meshed distribution network is converted into a radial network, by selecting break points. The branch current interrupted by the creation of every break point can be replaced by current injections at its two nodes without affecting the network operating conditions. Sparse methods cannot be applied being a Z-Bus based method [9].

II. TOPOLOGY BASED LOAD FLOW SOLUTION

Equivalent current injection: For distribution systems, the models which are based on the equivalent current injection as reported by Shirmohammadi et al., (1988), Chen et al. (1991.) and Teng and Lin (1994) are more convenient to use. At each bus 'k' the complex power S_k is specified by,

$$S_i = P_i + j Q_i \quad (1)$$

Corresponding equivalent current injection at the k-th iteration of the solution is given by,



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Website: www.ijareeie.com

Vol. 6, Issue 12, December 2017

$$I_i^k = I_i^r(V_i^k) + jI_i^i(V_i^k) = \left(\frac{P_i + jQ_i}{V_i^k} \right)^* \quad (2)$$

V_i^k is the node voltage at the kth iteration.

I_i^k is the equivalent current injection at the k-th iteration.

I_i^r and I_i^i are the real and imaginary parts of the equivalent current injection at the k-th iteration respectively.

Bus-Injection to Branch-Current matrix : (BIBC)

The power injections can be converted into equivalent current injections using the equation(1). The set of equations can be written by applying Kirchoff's current law (KCL) to the distribution network. Then the branch currents can be formulated as a function of the equivalent current injections.

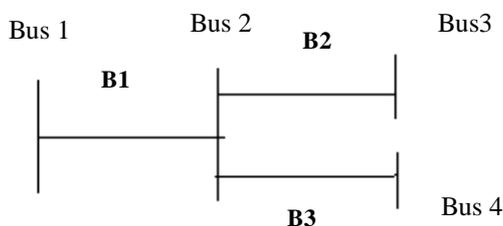


Fig. 1 Sample distribution system.

$$\begin{aligned} B_1 &= I_3 + I_4 \\ B_2 &= I_3 \\ B_3 &= I_4 \end{aligned}$$

Where, I_2 , I_3 and I_4 are load currents respectively at buses 2, 3 and 4

$$[B] = [BIBC] [I] \quad (3)$$

$$\begin{bmatrix} B_1 \\ B_2 \\ B_3 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} I_2 \\ I_3 \\ I_4 \end{bmatrix}$$

The constant BIBC matrix has non-zero entries of +1 only. For a distribution system with m-branch sections and n-buses, the dimension of the BIBC is $m \times (n-1)$.

Branch-Current to Bus-Voltage Matrix :

The relation between the branch currents and bus voltages can be obtained by following equations.

$$\begin{aligned} V_2 &= V_1 - B_1 Z_{12} \\ V_3 &= V_2 - B_2 Z_{23} \end{aligned}$$

where V_2 , V_3 are the voltages at node 2 and node 3. Z_{23} is the impedance between 2 and 3 nodes. The above equations can also be written as ,

$$\begin{aligned} V_1 - V_2 &= Z_{12} B_1 \\ V_1 - V_3 &= Z_{12} B_1 + B_2 Z_{23}. \end{aligned}$$

In general, $[V_1] - [V_k] = [Z] [B]$ where Z matrix will have elements in the transposed matrix of BIBC matrix. V_1 matrix contains all elements equal to 1.0pu.

$$[\Delta V] = [BCBV][B] \quad (4)$$

That can be written as,

$$\begin{bmatrix} V_1 \\ V_1 \\ V_1 \end{bmatrix} - \begin{bmatrix} V_2 \\ V_3 \\ V_4 \end{bmatrix} = \begin{bmatrix} Z_{12} & 0 & 0 \\ Z_{12} & Z_{23} & 0 \\ Z_{12} & 0 & Z_{24} \end{bmatrix} \begin{bmatrix} B_1 \\ B_2 \\ B_3 \end{bmatrix} \quad (5)$$

$$[\Delta V] = [BCBV][BIBC][I] \quad (6)$$

That can be written as,



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Website: www.ijareeie.com

Vol. 6, Issue 12, December 2017

$$\begin{bmatrix} V_1 \\ V_1 \\ V_1 \end{bmatrix} - \begin{bmatrix} V_2 \\ V_3 \\ V_4 \end{bmatrix} = \begin{bmatrix} Z_{12} & \mathbf{0} & \mathbf{0} \\ Z_{12} & Z_{23} & \mathbf{0} \\ Z_{12} & \mathbf{0} & Z_{24} \end{bmatrix} \begin{bmatrix} 1 & 1 & 1 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} I_2 \\ I_3 \\ I_4 \end{bmatrix} \quad (7)$$

2.1 Algorithm for Topology based Load Flow Method

1. Read the system data,
2. Build BIBC matrix as given in equation (3).
3. Transpose BIBC and multiply with impedances and obtain BCBV matrix as given in eq. (7).
4. Initialize iteration count =1. Calculate equivalent current injections using equation(2). Considering uniform voltage profile of 1 pu at all buses.
5. Obtain ΔV matrix using equation (4).
6. Obtain voltages at all nodes.
7. Calculate current injections using new set of voltages.
8. If the difference in currents between current iteration currents and previous iteration currents is greater than 0.001, then print the result, otherwise, increment of the count and repeat the procedure from step(4).

As already presented in the previous sections, two important steps involved in this algorithm are, $[B] = [BIBC][I]$: matrix $[I]$ is current injections. Branch currents expressed in terms of bus current injections.

$[\Delta V] = [BCBV][B]$: Voltage deviations expressed in terms of branch currents.

$I_i^k = I_i^r(V_i^k) + jI_i^i(V_i^k) = \left(\frac{P_i + jQ_i}{V_i^k}\right)^*$ Conversion of Power injections into current injections. From the above two equations, $[\Delta V] = [BCBV][BIBC][I]$

2.2 Load Modeling : The modeling of various types of loads are presented in this section. The general expression of load is shown below. The values of constants will be different for different loads.

$$P = P_o(a_0 + a_1V + a_2V^2 + a_3V^{e_1})$$

$$Q = Q_o(b_0 + b_1V + b_2V^2 + b_3V^{e_2})$$

Table 1 : Values of coefficients for different types of loads.

Type of load	a_0	b_0	a_1	b_1	a_2	b_2	a_3	b_3	e_1	e_2
Constant Power Load	1	1								
Constant Current Load			1	1						
Constant Impedance Load					1	1				
Composite load	0.4	0.4	0.3	0.3	0.3	0.3				
Exponential load							1	1	1.38	3.22

2.3 Calculation of current for different types of loads :

Major part of the program is similar except that the calculation of current is different for different types of loads. It is described in this section.

For Constant Power load : `currents=conj((p+q*i)./v);`

For Constant Current load : `currents=conj((p.*v+q.*v*i)./v);`



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

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Vol. 6, Issue 12, December 2017

For Constant Impedance load : $\text{currents} = \text{conj}((p \cdot (v.^2) + q \cdot (v.^2) \cdot i) ./ v);$

For Composite load :

$p = p \cdot (0.4 + 0.3 \cdot v + 0.3 \cdot v.^2)$

$q = q \cdot (0.4 + 0.3 \cdot v + 0.3 \cdot v.^2)$

$\text{currents} = \text{conj}(p + q \cdot i ./ v);$

For Exponential load : $\text{currents} = \text{conj}((p \cdot (v.^{1.38}) + q \cdot (v.^{3.22}) \cdot i) ./ v);$

III. LOAD FLOW RESULTS FOR DIFFERENT TYPES OF LOADS

The load flow solution is obtained for constant power load, constant current load, constant impedance load, composite and exponential loads. For various types of loads, loadflow solution is obtained on 15 Bus, 33 Bus, 69 Bus and 85 Bus Systems. Sample program is presented in the Appendix 5. Data for the loadflow for 15 Bus, 33 Bus, 69 Bus and 85 Bus Systems is presented in Appendix 1 to Appendix 4 respectively. For 15 Bus system, 33 Bus system and 85 bus systems, the base voltage is 11 kV and base MVA is 100 MVA. For 69 bus system, base Voltage and base MVA are 12.66 kV and 100 MVA

Table 2 : Power Loss and Minimum voltage for 15-Node network

Type of load	Power loss		Minimum voltages(p.u)
	Real(KW)	Reactive(KVAr)	
CP	61.7803	57.30	0.9445
CI	56.142	52.05	0.9472
CZ	51.46	47.69	0.9496
Composite	56.73	50.31	0.9496
Exponential	50.26	46.59	0.9501

Table 3 : Power Loss and Minimum Voltage for 33-Node network

Type of load	Power loss		Minimum voltages(p.u)
	Real(kw)	Reactive(kVAr)	
CP	295.83	200.5	0.8684
CI	241.87	163.2	0.8825
CZ	205.80	138.2	0.8928
Composite	248.1	167.9	0.8785
Exponential	207.2	139.8	0.888



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Website: www.ijareeie.com

Vol. 6, Issue 12, December 2017

Table 4 : Power Loss and Minimum Voltage for 69-Node network

Type of load	Power loss		Minimum voltages(p.u)
	Real(kw)	Reactive(kVAr)	
CP	224.78	102.11	0.9092
CI	191.50	87.80	0.9164
CZ	166.98	77.24	0.9219
Composite	195.22	89.43	0.9158
Exponential	170.36	78.66	0.9207

Table 5 : Power Loss and Minimum Voltage for 85-Node network

Type of load	Power loss		Minimum voltages(p.u)
	Real(kw)	Reactive(kVAr)	
CP	224.78	198.53	0.8713
CI	253.68	159.63	0.8854
CZ	212.248	133.90	0.8956
Composite	260.58	163.95	0.8883
Exponential	202.85	128.49	0.8959

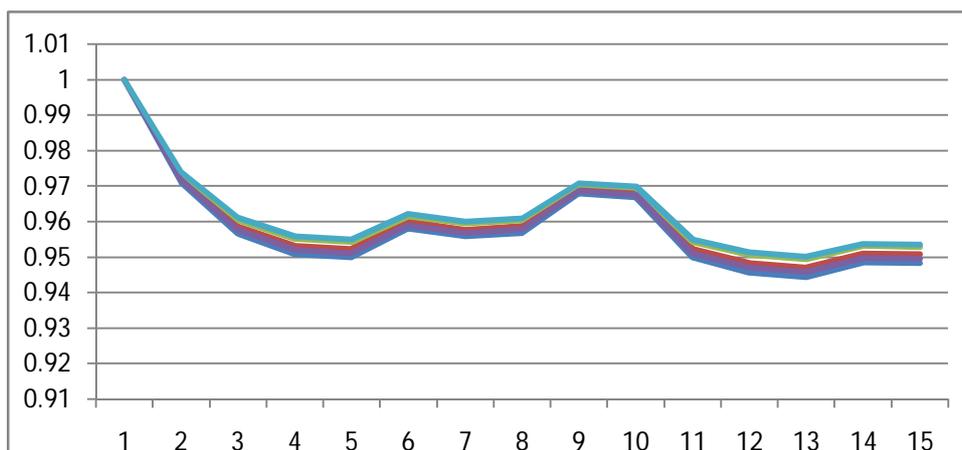


Fig.2 : Voltages on 15 Bus system



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Vol. 6, Issue 12, December 2017

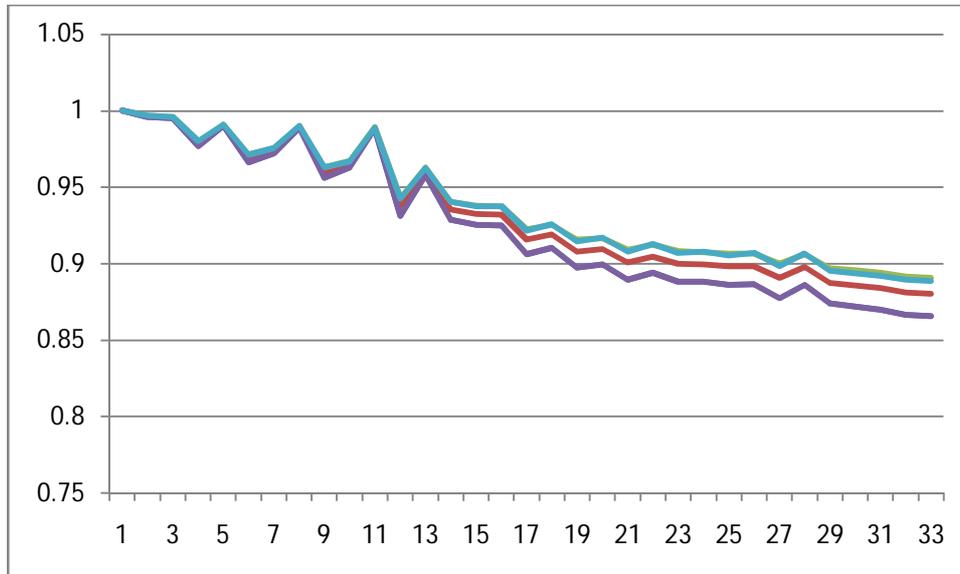


Fig.3 : Voltages on 33 Bus system

Table 6 : Voltages on 15 Bus System for various types of loads

Bus No	Constant Power Load	Constant Current Load	Constant Impedance Load	Composite Load	Exponential load
1	1	1	1	1	1
2	0.9713	0.9726	0.9737	0.9719	0.974
3	0.9567	0.9587	0.9605	0.9577	0.961
4	0.9509	0.9532	0.9553	0.9521	0.9558
5	0.9499	0.9523	0.9544	0.9511	0.9549
6	0.9581	0.96	0.9616	0.959	0.9621
7	0.9559	0.9578	0.9596	0.9568	0.96
8	0.9568	0.9588	0.9604	0.9578	0.9609
9	0.9679	0.9694	0.9706	0.9687	0.9709
10	0.9669	0.9683	0.9696	0.9676	0.9699
11	0.9499	0.9523	0.9544	0.9511	0.9549
12	0.9457	0.9484	0.9507	0.947	0.9513
13	0.9444	0.9471	0.9495	0.9458	0.9501
14	0.9486	0.9511	0.9532	0.9498	0.9537
15	0.9484	0.9509	0.953	0.9496	0.9536



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

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Vol. 6, Issue 12, December 2017

Table 7 : Voltages on 33 Bus System for various types of loads

Bus No	Constant Power	Constant Current	Constant Impedance	Composite	Exponential load
1	1	1	1	1	1
2	0.996	0.9963	0.9965	0.996	0.9965
3	0.9952	0.9955	0.9958	0.9952	0.9957
4	0.9767	0.9786	0.98	0.9767	0.9799
5	0.9902	0.9906	0.9909	0.9902	0.9909
6	0.9664	0.9693	0.9715	0.9664	0.9713
7	0.9719	0.9739	0.9755	0.9719	0.9753
8	0.9892	0.9896	0.9899	0.9892	0.9899
9	0.9561	0.9601	0.9631	0.9561	0.9628
10	0.9627	0.9652	0.967	0.9627	0.9668
11	0.9883	0.9887	0.989	0.9883	0.9889
12	0.9314	0.938	0.9429	0.9314	0.9425
13	0.9581	0.9608	0.9628	0.9581	0.9625
14	0.9286	0.9355	0.9406	0.9286	0.9403
15	0.9253	0.9325	0.9379	0.9253	0.9374
16	0.9249	0.9322	0.9376	0.9249	0.9374
17	0.9064	0.9158	0.9228	0.9064	0.9218
18	0.9102	0.9191	0.9256	0.9102	0.9257
19	0.8976	0.9081	0.9158	0.8976	0.9146
20	0.8994	0.9095	0.9169	0.8994	0.9172
21	0.8894	0.901	0.9094	0.8894	0.9079
22	0.8941	0.9047	0.9126	0.8941	0.9131
23	0.8883	0.9	0.9085	0.8883	0.907
24	0.8881	0.8994	0.9078	0.8881	0.9081
25	0.8863	0.8983	0.907	0.8863	0.9054
26	0.8868	0.8982	0.9067	0.8868	0.907
27	0.8776	0.8907	0.9002	0.8776	0.8984
28	0.8863	0.8979	0.9064	0.8863	0.9067
29	0.874	0.8876	0.8974	0.874	0.8955
30	0.8719	0.8857	0.8958	0.8719	0.8937
31	0.8699	0.884	0.8942	0.8699	0.8921
32	0.8667	0.8812	0.8917	0.8667	0.8895
33	0.8658	0.8804	0.891	0.8658	0.8888



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Vol. 6, Issue 12, December 2017

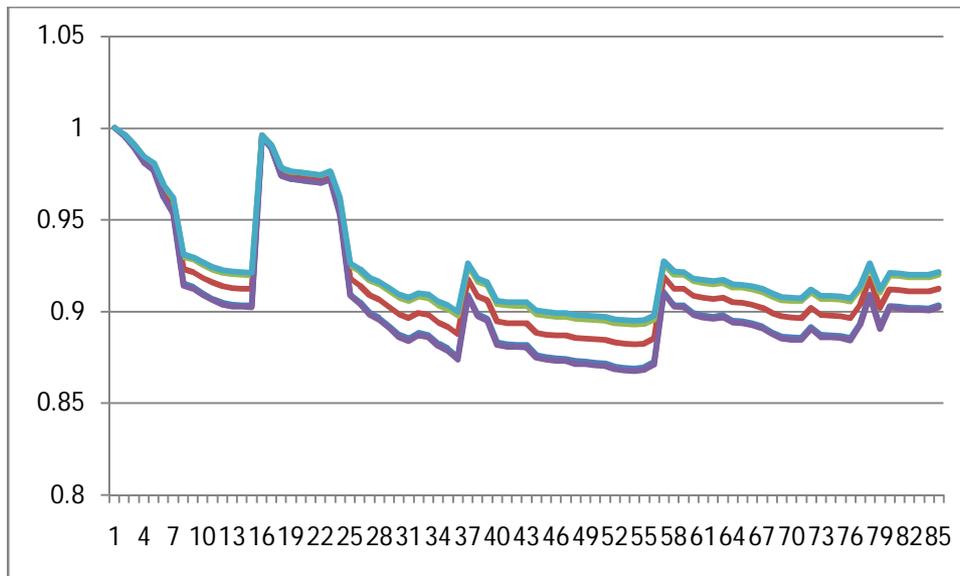


Fig.4 : Voltages on 85 Bus system

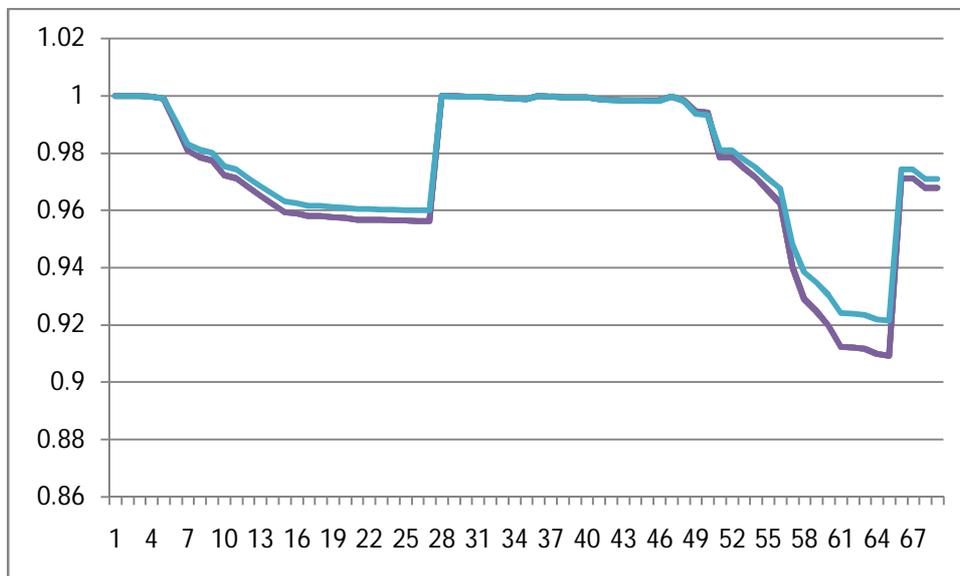


Fig.5 : Voltages on 69 Bus system

IV.CONCLUSIONS

The load flow solution is obtained for constant power load, constant current load, constant impedance load, composite and exponential loads. For various types of loads, load flow solution is obtained on 15 Bus, 33 Bus, 69 Bus and 85 Bus Systems. The obtained results are in close agreement with the results obtained in literature.

It is observed that on all the bus systems, lowest minimum voltage is obtained for constant power loads. For constant power loads, on 15 Bus system, minimum voltage obtained is 0.9445 pu, on 33 Bus system minimum voltage is 0.8684 pu, on 69 Bus system minimum voltage is 0.9092 pu and on 85 bus system, minimum voltage for constant power load is 0.8713 pu.



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Better voltage profile is observed with exponential loads on 15 bus and 85 bus systems. The minimum voltages on 15 bus system is 0.9501 pu and on 85 bus system is 0.8959 pu. On 33 bus and 69 bus systems, better voltage profile is observed with constant impedance loads. On 33 Bus system, minimum voltage is 0.8928 pu and on 69 bus system is 0.922 pu

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